Effect of calcination temperature and reaction conditions on methane partial oxidation using lanthanum-based perovskite as oxygen donor

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Abstract: We investigated the effect of calcination temperature, reaction temperature, and different amounts of replenished lattice oxygen on the partial oxidation of methane (POM) to synthesis gas using perovskite-type LaFeO3 oxide as oxygen donor instead of gaseous oxygen, which was prepared by the sol-gel method, and the oxides were characterized by XRD, TG/DTA, and BET. The results indicated that the particle size increased with the calcination temperature increasing, while BET and CH4 conversion declined with the calcination temperature increasing using LaFeO3 oxide as oxygen donor in the absence of gaseous oxygen. CO selectivity remained at a high level such as above 92%, and increased slightly as the calcination temperature increased. Exposure of LaFeO3 oxides to methane atmosphere enhanced the oxygen migration of in the bulk with time online owing to the loss of lattice oxygen and reduction of the oxidative stated Fe ion simultaneously. The high reaction temperature was favorable to the migration of oxygen species from the bulk toward the surface for the synthesis gas production with high CO selectivity. The product distribution and evolution for POM by sequential redox reaction was determined by amounts of replenished lattice oxygen with gaseous oxygen. The optimal process should decline the total oxidation of methane, and increase the selectivity of partial oxidation of methane.

Keywords: perovskite LaFeO3; lattice oxygen; synthesis gas; redox reaction; rare earths

1 Experimental

1.1 Catalyst preparation

A sol-gel method was employed to prepare the samples. Powders of La(NO3)3·6H2O (>99%, Beijing Chemical Company), Fe(NO3)3·9H2O (>99%, Beijing Chemical Company) were weighed to achieve equimolar amounts and dissolved in a small amount of distilled water. Glycine (>99%, Beijing Chemical Company) was kept at a ratio of NH3/NO3 = 1.05 to prepare the gel, where NH3 originated from glycine, and NO3 originated from La(NO3)3·6H2O and Fe(NO3)3·9H2O. Gelation was induced by heating the solution at 80–90 °C; this temperature was maintained for 10 h, then heated to 250 °C and kept for 30 min with a fast decomposition reaction, upon which a dried powder precursor...
was obtained. Thus, obtained portions of such precursor were then fired in a muffle oven at different temperatures (namely, 800, 900, 1000, and 1100 °C for 6 h) at a heating rate of 10 °C/min.

1.2 Catalyst characterization

Thermal decomposition of LaFeO$_3$ precursor was investigated by thermogravimetry (TG, Setaram, Labsys). In a typical measurement, 30 mg of sample was heated in an Al$_2$O$_3$ crucible at a constant heating rate of 10 °C/min from 60 °C to 1200 °C, with air purging at a flow rate of 30 ml/min. Powder X-ray diffraction (XRD) patterns were recorded from 2θ=20° to 80° at a speed of 4 (°)/min and 0.02° step size using a ShiDU XRD-6000 powder diffractometer employing Ni-filtered Cu Kα radiation. The crystallite size of the samples was calculated from the full width at half maximum of the most intense diffraction peak using Scherrer’s equation.

The specific surface area of the samples was determined by applying the BET method to nitrogen adsorption isotherms recorded at −196 °C, using a Quantachrome NOVA-1200 gas absorption analyzer.

1.3 Catalytic performance by continuous flow reaction

Catalytic performance was investigated in CH$_4$/Ar over 0.25 g LaFeO$_3$ oxides at 900 °C by continuous flow reaction. The samples were pretreated in an O$_2$ flow (O$_2$/Ar=11%), total flow rate=23 ml/min) at reaction temperature for 30 min. Then the gas was switched to pure Ar (total flow rate=23 ml/min) for about 30 min for removing gas phase oxygen. Finally, the gas was switched to 11% CH$_4$/He (mol, total flow rate=23 ml/min) for the reaction to occur.

1.4 Sequential redox reaction for replenished lattice oxygen

The amount of replenished lattice oxygen with gaseous oxygen, which was determined by preliminary experiments, was controlled by sequential redox reaction between reductive (CH$_4$/He) and oxidative atmospheres (O$_2$/Ar) in a fixed-bed reactor. The 0.25 g samples reacted with methane first, then switched to O$_2$/He for replenishing the consumed oxygen species, and then switched to CH$_4$/Ar at 900 °C. The total gas flow rate was 25 ml/min. Ar/He was used as dilution gas and tracer gas. The ratios of the amount of replenished lattice oxygen and that of the full oxidation were 20%, 40%, 60%, 80%, and 100%, respectively.

The reactant and products were detected using the mass spectrometer (m/e: 2 (H$_2$), 15 (CH$_4$), 18 (H$_2$O), 28 (CO), 32 (O$_2$), and 44 (CO$_2$), where, m/e indicates the mass to charge ratio. The pure CH$_4$, CO, H$_2$, and CO$_2$ pulses were injected to calculate the amount of CH$_4$, CO, and CO$_2$ on the oxides taking into account a previous calibration of the mass spectrometer. The calibration of the mass spectrometer was carried out with standard gas mixtures (known composition). The cracking coefficients of methane, CO, and CO$_2$ were determined and used to calculate their concentrations. The CO selectivity was defined as CO/(CO+CO$_2$)×100%.

2 Results and discussion

2.1 Influence of calcination temperature on crystallization and catalytic performance

Fig.1 displays the TG/DTA curves for the powder precursor obtained after a fast decomposition reaction at 250 °C for 30 min (see Experimental). A relatively small weight loss (of ca. 5.2%) is observed between 60 and ca. 555 °C, in correlation with a broad exothermic peak. After the decomposition reaction at 250 °C for 30 min, water and most of the Glycine is removed, but a substantial amount of glycine can remain adsorbed on the gel, which is ascribed to the burning of the residual organic components[9]. An apparent weight loss (ca. 4.8%) is produced between ca. 582 and 900 °C in coincidence with the observation of a relatively large exothermic peak, which shows the formation of a crystalline phase oxide. This process most likely corresponds mainly to an oxygen loss resulting in the final generation of the perovskite phase[9].

The crystal structure of the samples calcined at different temperatures was analyzed by XRD (Fig.2). The results show that LaFeO$_3$ samples are single-phase perovskites (orthorhombic; Pnma space group), compared with the XRD data of the perovskite structure oxide (JCPDS card No. 37-1493; 2θ=32.190 (100%), 57.399 (39%), 46.144 (30%), 39.674 (18%), 22.606 (17%), 67.349 (15%), 78.641 (11%)). The crystalline size and intensity are, as expected, observed to increase with the calcination temperature increasing, and appear relatively small for the sample calcined at lower temperatures.
Further data for the crystalline LaFeO$_3$ phase extracted from these diffraction results are collected in Table 1. Practically, no obvious volume change is detected for this phase upon changing the calcination temperature while the primary particle size increases with increasing the calcination temperature, in qualitative agreement with the decrease in specific surface area.

Fig. 3 presents the results of the methane partial oxidation experiments performed by continuous flow reaction over LaFeO$_3$ oxide calcined at different temperatures for 6 h. It is observed that the lower the calcination temperature, the higher is the methane conversion that can be obtained. Especially, the higher the calcination temperature, the methane conversion declines more obviously, while CO selectivity remains at a high level above 92%, and increases slightly as the calcination temperature increases. The effects of calcination temperature for partial oxidation of methane are as follows: On one hand, it is favorable to produce more oxygen vacancies in which active oxygen are formed. On the other hand, the methane conversion drops because of the decrease of surface area as the calcination temperature increases, as shown in Table 1. The catalytic performance of the LaFeO$_3$ sample is relevant with the crystalline size and the rate of oxygen migration from bulk toward surface. Another side is that oxygen vacancy order to disorder transition occurs when temperature increases, which can decrease the mobility of oxygen species in the bulk[9,10], and result in the decreasing methane conversion.

From Fig.4, the oxygen amount of every 50 s cumulative data for CO formation at different calcination temperatures is the highest at lower calcination temperature. As the contact time with methane increases, the total oxygen amount for CO formation increases. The amount of oxygen of every 50 s cumulative data for CO formation increases with time on line, especially for the LaFeO$_3$ oxide of high calcination temperature (Table 2), which indicates that the effects of calcination temperature on the methane partial oxidation are significant.

### Table 1: Crystalline size and BET area for LaFeO$_3$ samples calcined at different temperatures

<table>
<thead>
<tr>
<th>Calcination conditions</th>
<th>Crystalline size (nm)</th>
<th>Unit cell volume ($\text{nm}^3$)</th>
<th>BET area ($\text{m}^2/\text{g}$)</th>
</tr>
</thead>
<tbody>
<tr>
<td>800 °C, 6 h</td>
<td>31.7</td>
<td>0.24468</td>
<td>12.56</td>
</tr>
<tr>
<td>900 °C, 6 h</td>
<td>40.0</td>
<td>0.24474</td>
<td>8.56</td>
</tr>
<tr>
<td>1000 °C, 6 h</td>
<td>50.7</td>
<td>0.24438</td>
<td>4.14</td>
</tr>
<tr>
<td>1100 °C, 6 h</td>
<td>53.5</td>
<td>0.24341</td>
<td>2.36</td>
</tr>
</tbody>
</table>

### Table 2: Oxygen amount of every 50 s cumulative data for CO formation at different calcination temperatures

<table>
<thead>
<tr>
<th>Temperature/°C, Time/s</th>
<th>0–50</th>
<th>50–100</th>
<th>100–150</th>
<th>150–200</th>
<th>200–250</th>
<th>250–300</th>
</tr>
</thead>
<tbody>
<tr>
<td>800</td>
<td>64.65</td>
<td>61.18</td>
<td>58.02</td>
<td>59.28</td>
<td>60.86</td>
<td>59.67</td>
</tr>
<tr>
<td>900</td>
<td>50.18</td>
<td>56.98</td>
<td>57.68</td>
<td>58.75</td>
<td>60.67</td>
<td>60.02</td>
</tr>
<tr>
<td>1000</td>
<td>33.00</td>
<td>39.34</td>
<td>44.64</td>
<td>46.67</td>
<td>50.15</td>
<td>50.69</td>
</tr>
<tr>
<td>1100</td>
<td>28.45</td>
<td>30.69</td>
<td>36.84</td>
<td>42.72</td>
<td>48.64</td>
<td>54.93</td>
</tr>
</tbody>
</table>

2.2 Effects of reaction temperature over LaFeO$_3$ oxide by continuous flow reaction

The typical product distribution over LaFeO$_3$ perovskite in Fig.5 indicates that the reactions are initially very fast and produce significant quantities of carbon dioxide and water, originating from the total oxidation of methane at the preliminary stage. When oxygen species in the surface is consumed, carbon dioxide formation declines rapidly to a very low level, while methane intensity quickly declines, which indicates that methane conversion is sharply enhanced. CO and H$_2$ intensities increase steadily with time, while the CH$_4$ intensity decreases gradually, and the synthesis gas is the dominant product. It is noted that the consumption of lattice oxygen on the surface enhances the oxygen mobility from the bulk toward the surface according to the change of the CO slope, which is relevant to the loss of lattice oxygen and reduction of the oxidation state of the Fe ion simultaneously$^{[11,12]}$. To facilitate the qualitative comparison of the migration rate of lattice oxygen at different temperatures, the CO response is presented in Fig.6, respectively. From Fig.6, it can be seen that the amount of CO increases sharply when the reaction temperature increases from 700 to 950 $^\circ$C, owing to the higher migration rate of lattice oxygen at high temperature, but the intensity of CO decreases first at high reaction temperature (950 $^\circ$C). The overall oxygen migration in LaFeO$_3$ oxide will be controlled by the interaction between processes: oxygen diffusion in bulk phase and reaction with the methane at the surface. Hence, the mobility of lattice oxygen plays an important role in the partial oxidation of methane without gaseous oxygen. The migration rate of oxygen during the CH$_4$ reaction with LaFeO$_3$ oxide is strongly affected by the reaction temperature. The intensity of CO increases with reaction temperature, and considerably more CH$_4$ is selectively oxidized to CO and H$_2$ at high temperatures. The rate of oxygen migration from bulk to surface increases with rising temperature, and more amounts of CO and H$_2$ are formed.

2.3 Effect of different amounts of replenished lattice oxygen over LaFeO$_3$ oxide by sequential redox reaction

The oxidation of hydrocarbons was supposed to occur on the perovskite surface by both suprafacial and intrafacial reaction$^{[13]}$, which involved lattice oxygen in the bulk without gaseous oxygen, and the migration rate of oxygen in the bulk became more and more important for catalytic performance over LaFeO$_3$ perovskite as oxygen donor. The results over LaFeO$_3$ oxide of different amounts of replenished lattice oxygen are shown in Fig.7.

The product profiles in the switch reaction from O$_2$/Ar to CH$_4$/He on LaFeO$_3$ oxide are shown in Fig.7. There is delay between H$_2$, CO and H$_2$O, CO$_2$ over LaFeO$_3$ oxide of fully replenished lattice oxygen. With the concentration of surface oxygen declining, H$_2$ and CO appear over LaFeO$_3$ oxide in the absence of gaseous oxygen. The CO$_2$ and H$_2$O are formed first, then CO and H$_2$ are detected for the switch reaction over LaFeO$_3$ oxide of fully replenished lattice oxygen; however, the intensity of CO$_2$ does not decline immediately when the CO begins to be detected. There is an initial induction period over LaFeO$_3$ oxide of fully replenished lattice oxygen. However, the CO and H$_2$ form immediately, and the delay is hardly observed between H$_2$, CO and CO$_2$, H$_2$O over LaFeO$_3$ oxide of low amount of replenished lattice oxygen. It is noted that the slope of the CO curve decreases

Fig.5 Typical curves of product formation and reagent consumption during continuous flow reaction over fresh LaFeO$_3$ perovskite at reaction temperature 900 $^\circ$C

Fig.6 CO responses switch from He to CH$_4$/Ar at different reaction temperatures over LaFeO$_3$ oxide
slightly as the amounts of replenished lattice oxygen increase. The oxygen species is believed to be transported by both the surface reaction and the bulk ion conduction mechanism\textsuperscript{[15]}. Generally, the synthesis gas formation was favored by the rapid dissociation of methane, which proceeds apparently easier on the reduced surface containing metal/carbide clusters or nuclei\textsuperscript{[15]}, but the migration of oxygen species from the bulk toward the surface probably prevents the formation of nuclei of the reduced phases at the surface, and the migration rate of oxygen species in the bulk of oxide depends on the crystalline defect of the bulk of oxide\textsuperscript{[16]}. The oxygen species for the CO\textsubscript{2} formation can be described as surface anionic vacancies after the reaction of lattice oxygen from the surface. Thereafter, the synthesis gas formation proceeds via the migration of lattice oxygen from the bulk to the surface, which is confirmed by the previous article\textsuperscript{[15]}. The product distribution and evolution for POM by sequential redox reaction is determined by the amounts of replenished lattice oxygen with gaseous oxygen.

3 Conclusion

The effects of calcination temperature, reaction temperature, and different amounts of replenished lattice oxygen on methane partial oxidation (POM) over perovskite-type LaFeO\textsubscript{3} oxide prepared by the sol-gel method were investigated by the continuous flow reaction and the sequential redox reaction. The particle size and BET surface area were affected significantly by the calcination temperature. The CH\textsubscript{4} conversion declined with calcination temperature increase, while the CO selectivity remained at a high level of 92\%, and increased slightly as the calcination temperature increased. The higher reaction temperature was favorable to the conversion of CH\textsubscript{4} to synthesis gas with high selectivity, and enhanced the migration rate of oxygen species from the bulk toward the surface. The product distribution for POM by sequential redox reaction was determined by the amounts of replenished lattice oxygen with gaseous oxygen. Therefore, the process for synthesis gas production by sequential redox reaction using oxygen donor in the absence of gaseous oxygen could be optimized by controlling appropriate amounts of replenished lattice oxygen with gaseous oxygen.

References:

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